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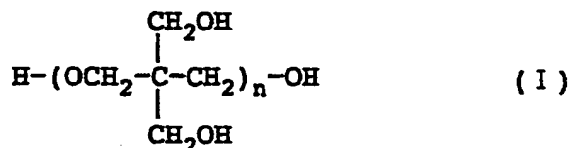
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(54) Refrigeration lubricants.

(57) A lubricant for hydrofluorocarbon refrigerant comprises as a main component an ester obtained by esterifying at least one straight or branched-chain monovalent fatty acid having a particular carbon number with neopentyl glycol or at least one compound of general formula (I) or a polyvalent alcohol of general formula (II) or further at least one polybasic acid having a particular carbon number:

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This lubricant has a sufficient compatibility with the hydrofluorocarbon refrigerant used as a refrigerant instead of the conventional chlorine-containing compounds.

REFRIGERATION LUBRICANTS

This invention relates to lubricants used with refrigerants, and more particularly to lubricants suitable for use in the compression of refrigerants containing no chlorine such as hydrofluorocarbons (HFC), preferably HFC-134a (1,1,1,2-tetrafluoroethane) and the like.

Heretofore, compounds containing fluorine and chlorine as a constituent element such as R-11 (trichloromonofluoromethane), R-12 (dichlorodifluoromethane) as a chlorofluorocarbon (CFC), R-22 (monochlorodifluoromethane) as a hydrochlorofluorocarbon (HCFC) and the like have been used as a refrigerant for freezers, air conditioners, refrigerators and the like. In connection with recent problem on breakage of ozone layer, new refrigerants containing no chlorine such as HFC-134a and so on are proposed as a possible replacement for R-12, causing no breakage of ozone layer.

As a refrigeration lubricant, there are known many mineral-series and synthetic oils. However, it has been confirmed that these oils are very poor in the compatibility with HFC-134a and can not be applied thereto. Therefore, it is important to take a countermeasure on this problem at the present. Furthermore, the lubricity, electric insulating property, energy saving property, anti-wear performance, sealability, thermal stability, prevention of sludge formation and the like are mentioned as performances required in the refrigeration lubricant, so that they are required to be considered in the development of the above countermeasure.

Incidentally, there have hitherto been known polyether series synthetic lubricants as a synthetic oil, which are reported in Journal of the Oil Chemistry, vol. 29, No. 8, pp 336-343 (1980) and Journal of the Petroleum Technology, vol. 8, No. 6, pp 562-566 (1985). Furthermore, Japanese Patent laid open No. 61-281199 describes a mixture of polyglycol represented by a general formula of $R_1[O-(R_2O)_m-R_3]_n$, an alkylbenzene and the like, and Japanese Patent laid open No. 57-63395 describes an oil obtained by mixing a polyether such as high molecular weight polyoxypropylene monobutyl ether with an epoxycycloalkyl compound, and Japanese Patent laid open No. 59-117590 describes a high viscosity mixed oil of a polyether compound and a paraffinic or naphthanic mineral oil.

However, the conventional synthetic lubricants as mentioned above can not be a refrigeration lubricant using HFC-134a as a refrigerant from a viewpoint of compatibility and the like.

In US Patent No. 4,755,316, polyoxyalkylene glycol (hereinafter abbreviated as PAG) having hydroxyl groups (-OH) at both terminals is reported as a refrigeration lubricant using HFC-134a. Further, it is described that PAG is dissolved in HFC-134a within a wide temperature range as compared with general PAG containing hydroxyl group and alkyl group at its terminals, whereby the recycle of the lubricant into a compressor is improved in the refrigeration system and the seizing in the actuation of the compressor at high temperature is prevented. Moreover, the temperature range compatible with HFC-134a is described to be between -40°C and $+50^{\circ}\text{C}$.

On the contrary, HFC-134a is a replacing refrigerant of R-12 and is mainly expected for use in a car air conditioner, a refrigerator and the like. In case of the refrigerator, it is required to have a good compatibility between lubricant and refrigerant, and further the lubricant itself is necessary to have an electric insulating property because the motor is substantially existent in the refrigeration system. However, the conventional compounds examined as a lubricant for HFC-134a refrigerant inclusive of PAG disclosed in US Patent No. 4,755,316 are remarkably poor in the electric insulating property as compared with the conventional refrigeration mineral oil and high in the hygroscopicity.

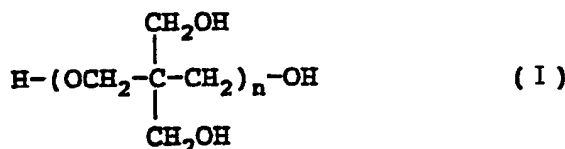
It is, therefore, an object of the invention to provide a refrigeration lubricant having an excellent compatibility with a new refrigerant such as HFC-134a or the like within a wide temperature range, a high electric insulating property and a low hygroscopicity.

At the present, a part of commercially available esters is used in systems using refrigerants R-12, R-22 and the like, but is incompatible with HFC-134a as a new refrigerant or is very narrow in the compatible range therewith. In this connection, the inventors have aimed at the fact that the ester has a high electric insulating property, a low hygroscopicity, a good lubricity and a high stability as compared with PAG and made various studies with respect to the molecule design of the ester showing a wide range of compatibility with HFC-134a, and found that only esters having a considerably restricted structure can be used in the HFC-134a refrigeration system, and as a result, the invention has been accomplished.

According to a first aspect of the invention, there is the provision of a lubricant for hydrofluorocarbon refrigerant such as HFC-134a and the like comprising as a main component an ester comprised of neopentyl glycol and at least one straight or branched-chain monovalent fatty acid having a carbon number of 3-18.

According to a second aspect of the invention, there is the provision of a lubricant for hydrofluorocarbon

refrigerant such as HFC-134a and the like comprising as a main component an ester comprised of at least one of pentaerythritol, dipentaerythritol and tripentaerythritol represented by the following general formula (I):



(in which n is 1, 2 or 3), and at least one straight or branched-chain monovalent fatty acid having a carbon number of 2-18.

According to a third aspect of the invention, there is the provision of a lubricant for hydrofluorocarbon refrigerant such as HFC-134a and the like comprising as a main component an ester comprised of a polyvalent alcohol represented by the following general formula (II):



(in which R is an alkyl group having a carbon number of not more than 3), at least one straight or branched-chain monovalent fatty acid having a carbon number of 2-18, and not more than 25 mol% per total fatty acid of at least one polybasic acid having a carbon number of 4-36.

In a preferred embodiment of the invention, the hydrofluorocarbon refrigerant is 1,1,1,2-tetrafluoroethane (HFC-134a).

The refrigeration lubricant for refrigerant HFC-134a and the like according to the first invention comprises an ester obtained by esterifying neopentyl glycol with at least one straight or branched-chain monovalent fatty acid having a carbon number of 3-18 as a main component.

In the first invention, the reason why the carbon number of the monovalent fatty acid is limited to 3-18 is due to the fact that when the carbon number is less than 3, the viscosity is too low, while when it exceeds 18, the resulting ester becomes cloudy or becomes very poor in the compatibility with the refrigerant HFC-134a and the like.

As the monovalent fatty acid, mention may be made of propionic acid, isopropionic acid, butanoic acid, isobutanoic acid, pentanoic acid, isopentanoic acid, hexanoic acid, heptanoic acid, isoheptanoic acid, octanoic acid, 2-ethyl hexanoic acid, nonanoic acid, 3,5,5-trimethyl hexanoic acid, decanoic acid, undecanoic acid, lauric acid, myristic acid, palmitic acid, palmitoleic acid, stearic acid, isostearic acid, oleic acid, and the like.

In the first invention, at least one of these monovalent fatty acids is properly mixed and esterified with neopentyl glycol to obtain an ester satisfying desirable physical properties required for various refrigerators.

In order to obtain a sufficiently satisfactory compatibility with the refrigerant HFC-134a and the like, it is preferable to use a mixture of straight chain fatty acid having a carbon number of 3-11, preferably 5-10 and a branched-chain fatty acid having a carbon number of 3-14, preferably 7-9 as the monovalent fatty acid. In this case, the amount of the straight or branched-chain fatty acid used is preferable to be not less than 50 mol% per the total monovalent fatty acid used.

According to the invention, in order to give a proper viscosity to the resulting ester, at least one polybasic acid having a carbon number of 4-36 may be esterified with neopentyl glycol in an amount of not more than 80 mol% per total fatty acid. Among the polybasic acids, considering the more compatibility with the refrigerant HFC-134a and the like and the physical properties of the resulting ester, a polybasic acid having a carbon number of 4-10 is preferable. Concretely, the polybasic acid includes succinic acid, glutaric acid, adipic acid, pimelic acid, suberic acid, azelaic acid, sebacic acid, phthalic acid, maleic acid, trimellitic acid and so on. Moreover, the polybasic acid having a carbon number of not more than 3 is a special product and is difficult to be cheaply available and is poor in the stability of the ester after the synthesis. While, when the carbon number exceeds 36, the compatibility of the resulting ester with HFC-134a and the like is largely lowered. In the invention, the reason why the amount of the polybasic acid added is limited to

not more than 80 mol% per the total fatty acid is due to the fact that when it exceeds 80 mol%, the gelation may be caused and it is difficult to obtain desirable physical properties.

The ester compounds according to the first invention can be obtained by the esterification reaction through dehydration reaction between the specified polyvalent alcohol and the specified fatty acid as mentioned above, or the general esterification reaction through an acid anhydride, an acid chloride or the like as a derivative of the fatty acid.

Since the ester according to the invention can be obtained by the above method, the remaining acid value and hydroxyl value are not particularly critical. However, when the acid value exceeds 3, there may be caused an unfavorable phenomenon that the metal soap is formed and precipitated by the reaction with a metal used inside the refrigerator, so that the acid value is preferable to be not more than 3. Furthermore, when the hydroxyl value exceeds 50, there may be caused an unfavorable phenomenon that the resulting ester becomes cloudy, so that the hydroxyl value is preferable to be not more than 50.

The lubricant for refrigerant HFC-134a and the like according to the second invention comprises an ester obtained by esterifying at least one of pentaerythritol, dipentaerythritol and tripentaerythritol represented by the aforementioned general formula (I) with at least one straight or branched-chain monovalent fatty acid having a carbon number of 2-18 as a main component.

In the condensate of pentaerythritol, the polymerization degree may be determined in accordance with the viscosity required in the resulting synthesized ester.

In the second invention, the carbon number of the monovalent fatty acid is limited to 2-18 because when it exceeds 18, the resulting ester becomes cloudy or becomes very poor in the compatibility with the refrigerant HFC-134a and the like.

As the monovalent fatty acid, mention may be made of acetic acid, propionic acid, isopropionic acid, butanoic acid, isobutanoic acid, pentanoic acid, isopentanoic acid, hexanoic acid, heptanoic acid, isooctanoic acid, octanoic acid, 2-ethyl hexanoic acid, nonanoic acid, 3,5,5-trimethyl hexanoic acid, decanoic acid, undecanoic acid, lauric acid, myristic acid, palmitic acid, palmitoleic acid, stearic acid, isostearic acid, oleic acid, linoleic acid, linolenic acid and the like.

In the second invention, at least one of these monovalent fatty acids is properly mixed and esterified with pentaerythritol or its condensate to obtain an ester satisfying desirable physical properties required for various refrigerators.

In order to obtain a sufficiently satisfactory compatibility with the refrigerant HFC-134a and the like, it is preferable to use a mixture of straight chain fatty acid having a carbon number of 3-11, preferably 5-10 and a branched-chain fatty acid having a carbon number of 3-14, preferably 7-9 as the monovalent fatty acid. In this case, the amount of the straight or branched-chain fatty acid used is preferable to be not less than 50 mol% per the total monovalent fatty acid used.

On the other hand, in order to give a proper viscosity to the resulting ester, at least one polybasic acid having a carbon number of 4-36 may be esterified with at least one of pentaerythritol, dipentaerythritol and tripentaerythritol in an amount of not more than 80 mol% per total fatty acid. In this case, the same polybasic acids as described in the first invention are used in the same manner as in the first invention.

The ester compounds according to the second invention can be obtained by the same method as in the first invention.

In the esters according to the second invention, the acid value is preferable to be not more than 3 and the hydroxyl value is preferable to be not more than 50 likewise the case of the first invention.

The lubricant for refrigerant HFC-134a and the like according to the third invention comprises an ester obtained by esterifying a polyvalent alcohol represented by the aforementioned general formula (II) with at least one straight or branched-chain monovalent fatty acid having a carbon number of 2-18 and not more than 25 mol% per total fatty acid of at least one polybasic acid having a carbon number of 4-36 as a main component.

When the carbon number of R in the general formula (II) is not less than 4, the compatibility of the resulting ester with HFC-134a and the like is largely lowered. As the polyvalent alcohol, mention may be made of trimethylol ethane, trimethylol propane, trimethylol butane and the like.

In the third invention, when the carbon number of the monovalent fatty acid is more than 18, it becomes very poor in the compatibility of the resulting synthesized ester with HFC-134a and the like. Particularly, the straight or branched-chain monovalent fatty acids having a carbon number of 3-10 are preferable. As the monovalent fatty acid, mention may be made of the same compounds as described in the second invention.

As to the polybasic acid, the polybasic acid having a carbon number of not more than 3 is a special product and is difficult to be cheaply available and is poor in the stability of the ester after the synthesis. While, when the carbon number exceeds 36, the compatibility of the resulting ester with HFC-134a and the like is largely lowered. Therefore, the carbon number of the polybasic acid is preferable to be 4-36, and

particularly the carbon number of 4-10 is favorable for ensuring the compatibility with HFC-134a at a wide range. As the polybasic acid, mention may be made of adipic acid, azelaic acid, sebacic acid and so on. Preferably, the monovalent fatty acid is 2-ethylhexanoic acid, and the polybasic acid is adipic acid.

Moreover, the reason why the amount of the polybasic acid added in the invention is limited to not more than 25 mol% per the total fatty acid is due to the fact that when it exceeds 25 mol% the gelation may be caused and it is difficult to obtain desirable physical properties.

The ester compounds according to the third invention can be obtained by the same method as in the first and second inventions. In any case, it is desirable that the ester does not contain carboxyl group.

The esters according to the invention exhibit a good compatibility with the refrigerant HFC-134a and the like over a wide range of from low temperature to high temperature as a lubricant for use in a refrigerator using HFC-134a as a refrigerant, whereby the lubricity and thermal stability of the refrigeration lubricant can be considerably improved. Furthermore, they are high in the electric insulating property and small in the hygroscopicity as compared with PAG conventionally examined as a refrigeration lubricant for HFC-134a. Therefore, the refrigeration lubricants comprising the ester according to the invention as a main component can solve the problems on the compatibility with HFC-134a and the hygroscopicity, which have never been solved in the conventional technique, and can further enhance the electric insulating property, which comes into problem when HFC-134a is used in a compressor for a refrigerator.

Moreover, additives usually used in the lubricant such as antioxidant, anti-wear agent, epoxy compound and the like may properly be added to the refrigeration lubricant according to the invention.

The following examples are given in illustration of the invention and are not intended as limitations thereof.

Examples 1-8, Comparative Examples 1-5

The performances as a refrigeration lubricant using HFC-134a as a refrigerant were evaluated with respect to eight esters A-1 - A-8 shown in the following Table 1 (all of which esters were not commercially available but were prepared according to the first invention). For the comparison, the same evaluation as mentioned above was made with respect to commercially available PAG (B-1 - B-3, made by Asahi Denka Co., Ltd.) and esters (C-1 - C-2, made by Nippon Oil and Fats Co., Ltd.) as a refrigeration lubricant shown in the following Table 2.

The lubricity, compatibility, thermal stability, electric insulating property and hygroscopicity as performances of the refrigeration lubricant for the compressor shown in Tables 1 and 2 were evaluated under the following conditions.

Lubricity

Seizuring load (Falex load-carrying capacity) was measured according to ASTM D-3233-73 under a controlled atmosphere of HFC-134a blown.

Compatibility

After 0.6 g of the test lubricant and 2.4 g of the refrigerant (HFC-134a) were sealed in a glass tube, the cooling at 1°C/min and the heating were carried out, during which a temperature causing two-phase separation was measured.

Thermal stability

After 1 g of the test lubricant, 1 g of the refrigerant (HFC-134a or R-12) and a catalyst (wire of iron, copper or aluminum) were sealed in a glass tube, the mixture was heated to 175°C, and a color of the lubricant after 10 days was judged by ASTM color system according to ANSI/ASHRAE 97-1983.

Electric insulating property

It was evaluated by a dielectric constant at 80 °C according to JIS C-2101.

Hygroscopicity

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Into a beaker of 100 ml was charged 60 g of the test lubricant, which was left to stand at a temperature of 25 °C and a humidity of 70% for 3 hours and then the water concentration was measured.

The evaluation results are shown in the following Table 3.

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Table 1

Item Ester	Straight chain fatty acid				Branched-chain fatty acid				Polybasic acid		Dynamic viscosity at 40°C (cSt)	Color (ASTM)
	C ₅	C ₈	C ₁₂	C ₁₈	C ₇	C ₈	C ₉	C ₁₈	adipic acid	sebacic acid		
A-1	30	20	-	-	-	50	-	-	-	-	4.6	L 0.5
A-2	30	-	10	10	50	-	-	-	-	-	7.0	L 0.5
A-3	10	-	-	10	40	-	40	-	-	-	14.4	L 0.5
A-4	-	20	-	-	75	-	-	5	-	-	6.5	L 0.5
A-5	-	5	10	-	-	75	-	-	10	-	11.9	L 0.5
A-6	-	10	-	-	65	-	-	-	-	25	20.9	L 0.5
A-7	-	-	-	-	-	100	-	-	-	-	7.4	L 0.5
A-8	-	10	-	-	40	-	10	-	40	-	22.1	L 0.5

Note) Amount of starting material was represented by mol%.

Table 2

	Type	Trade name	Color (ASTM)	Dynamic viscosity at 40 °C (cSt)
B-1	PAG 1	Adekapol M-30 1)	L 0.5	32.8
B-2	PAG 1	Adekapol M-110 2)	L 0.5	105.2
B-3	PAG 1	Adekapol MH-50 3)	L 0.5	54.6
C-1	ester	dioctyl sebacate	L 0.5	11.4
C-2	ester	Unistar MB-816 4)	L 0.5	8.1

1) polyoxypropylene glycol monoalkyl ether

2) polyoxypropylene glycol monoalkyl ether

3) polyoxyethylene propylene glycol monoalkyl ether

4) monoester of 2-ethylhexanol and palmitic acid

Table 3

	Test lubricant	Dielectric constant at 80 °C (p·cm)	Two-phase separation temperature (°C)		Seizuring load (Kgf)	Thermal stability				Hygroscopicity (water content, ppm)
			low temperature	high temperature		refrigerant R-12		refrigerant HFC-134a		
						color (ASTM)	sludge	color (ASTM)	sludge	
Acceptable Example	A-1	7.5 x 10 ¹²	≤-50 *	80≤ **	510	L 1.0	none	L 1.0	none	320
	A-2	6.1 x 10 ¹²	≤-50	80≤	519	L 1.0	none	L 1.0	none	335
	A-3	4.9 x 10 ¹³	≤-50	80≤	555	L 1.0	none	L 1.0	none	309
	A-4	1.7 x 10 ¹³	≤-50	80≤	541	L 1.0	none	L 1.0	none	317
	A-5	8.0 x 10 ¹²	-45	80≤	572	L 1.0	none	L 1.0	none	364
	A-6	5.8 x 10 ¹²	-41	80≤	603	L 1.0	none	L 1.0	none	371
	A-7	2.6 x 10 ¹³	≤-50	80≤	569	L 1.0	none	L 1.0	none	315
	A-8	4.8 x 10 ¹²	-36	80≤	648	L 1.0	none	L 1.0	none	330
Comparative Example	B-1	2.1 x 10 ⁷	≤-50	67	430	8.0≤	many	L 1.0	none	1600
	B-2	2.8 x 10 ⁷	insoluble	insoluble	480	8.0≤	many	L 1.0	none	1200
	B-3	≤10 ⁷	≤-50	53	430	8.0≤	many	L 1.0	none	2100
	C-1	5.1 x 10 ¹²	insoluble	insoluble	570	L 1.0	none	L 1.0	none	340
C-2	4.3 x 10 ¹²	insoluble	insoluble	590	L 1.0	none	L 1.0	none	365	

* : not higher than -50 °C

** : not lower than 80 °C

As seen from Table 3, when the esters according to the invention are compared with the conventional PGA (B-1 - B-3), the electric insulating property represented by the dielectric constant is 100,000 times or more and the two-phase separation at a high temperature is not caused. Furthermore, the seizing load is excellent and the hygroscopicity is low. The thermal stability is equal in case of the HFC-134a system, but is considerably excellent in case of the R-12 system. This is very advantageous in practical use because the mixing of HFC-134a and R-12 is not avoided at a stage of replacing the refrigerant from R-12 to HFC-134a.

On the other hand, when the esters according to the invention are compared with the commercially available esters (C-1 - C-2), the two-phase separation temperature is extremely different and the conventional esters are insoluble in HFC-134a. In this point, the molecule designed esters according to the invention have a great merit.

As seen from the above, the esters according to the invention are fairly excellent in the performances as a lubricant as compared with Comparative Examples.

Examples 9-17

The performances as a refrigeration lubricant using HFC-134a as a refrigerant were evaluated with respect to nine esters A-9 - A-17 shown in the following Table 4 (all of which esters were not commercially available but were prepared according to the second invention). The same evaluation as in Example 1 was made to obtain results as shown in the following Table 5.

Table 4

Item Ester	Polyvalent alcohol	Polybasic acid			Dynamic viscosity at 40°C (cSt)	Color (ASTM)
		straight chain fatty acid (mol%)	branched-chain fatty acid (mol%)	polybasic acid (mol%)		
A-9	pentaerythritol	—	isononanoic acid (100)	—	125.4	L 0.5
A-10	pentaerythritol	pentanoic acid (100)	—	—	14.5	L 0.5
A-11	pentaerythritol	propionic acid (70) stearic acid (30)	—	—	33.4	L 0.5
A-12	pentaerythritol	—	2-ethylhexanoic acid (100)	—	42.3	L 0.5
A-13	pentaerythritol	heptanoic acid (15)	isobutanoic acid (75)	adipic acid (10)	110.9	L 0.5
A-14	dipentaerythritol	propionic acid (30)	2-ethylhexanoic acid (70)	—	123.9	L 0.5
A-15	dipentaerythritol	isostearic acid (10)	isobutanoic acid (90)	—	68.4	L 0.5
A-16	dipentaerythritol	butanoic acid (95)	—	sebacic acid (5)	89.4	L 0.5
A-17	tripentaerythritol	propionic acid (20)	2-ethylhexanoic acid (80)	—	146.3	L 0.5

Note) Mol% is an amount per total acid.

Table 5

	Test lubricant	Dielectric constant at 80 °C ($\Omega \cdot \text{cm}$)	Two-phase separation temperature (°C)		Seizuring load (Kgf)	Thermal stability				Hygroscopicity (water content, ppm)
			low temperature	high temperature		refrigerant R-12		refrigerant HFC-134a		
						color (ASTM)	sludge	color (ASTM)	sludge	
Acceptable Example	A-9	6.5×10^{13}	-38	80 \leq	641	L 1.0	none	L 1.0	none	292
	A-10	1.2×10^{13}	≤ -50	80 \leq	524	L 1.0	none	L 1.0	none	319
	A-11	7.6×10^{12}	≤ -50	80 \leq	541	L 1.0	none	L 1.0	none	344
	A-12	1.7×10^{13}	≤ -50	80 \leq	549	L 1.0	none	L 1.0	none	331
	A-13	4.1×10^{12}	-43	80 \leq	610	L 1.0	none	L 1.0	none	348
	A-14	2.6×10^{12}	-40	80 \leq	623	L 1.0	none	L 1.0	none	325
	A-15	1.4×10^{13}	≤ -50	80 \leq	581	L 1.0	none	L 1.0	none	339
	A-16	5.1×10^{12}	≤ -50	80 \leq	602	L 1.0	none	L 1.0	none	358
	A-17	4.5×10^{12}	-31	80 \leq	654	L 1.0	none	L 1.0	none	324

As seen from Tabl 5, when the esters according to th invention are compared with the conventional
 PGA (B-1 - B-3) shown in Tables 2 and 3, the electric insulating property represented by the dielectric
 constant is 100,000 times or more and the two-phase separation at a high temperature is not caus d.
 5 Furthermore, the seizing load is excellent and the hygroscopicity is low. The thermal stability is equal in
 case of the HFC-134a system, but is considerably excellent in case of the R-12 system. This is very
 advantageous in practical use because the mixing of HFC-134a and R-12 is not avoided at a stage of
 replacing the refrigerant from R-12 to HFC-134a.

On the other hand, when the esters according to the invention are compared with the commercially
 10 available esters (C-1 - C-2) shown in Tables 2 and 3, the two-phase separation temperature is extremely
 different and the conventional esters are insoluble in HFC-134a. In this point, the molecule designed esters
 according to the invention have a great merit.

As seen from the above, the esters according to the invention are fairly excellent in the performances
 as a lubricant as compared with Comparative Examples.

15 The HFC-134a has been mentioned as a possible replacement for R-12 and is used for car air
 conditioner, refrigerator and the like. Particularly, in case of the car air conditioner, the compressor is driven
 in summer season, so that the compatibility between oil and refrigerant at high temperature becomes
 important. When the two-phase separation between oil and refrigerant is caused in the compressor during
 the driving, the refrigerant having a larger specific gravity remains in the lower portion of the compressor,
 20 resulting in the occurrence of compressor seizing.

In case of the refrigerator, the motor is included in the compressor, so that leakage of electricity comes
 into problem. In this connection, the esters according to the invention have a dielectric constant higher by
 100,000 times or more than that of the conventional PAG and are excellent in the electric insulating
 property, so that they can be said to be a refrigeration lubricant for the refrigerator.

25 Concretely, lubricants having a dynamic viscosity of 10-50 Cst at 40° C are used as a lubricant for the
 refrigerator requiring a two-phase separation temperature of not higher than -40° C, so that the esters A-10,
 A-11 and A-12 are particularly suitable therefor. On the other hand, lubricants having a dynamic viscosity of
 80-150 Cst at 40° C are used as a lubricant for the car air conditioner requiring a two-phase separation
 temperature of not higher than -20° C, so that the esters A-9, A-13, A-14, A-16 and A-17 are particularly
 30 suitable therefor.

Examples 18-25

35 The performances as a refrigeration lubricant using HFC-134a as a refrigerant were evaluated with
 respect to eight esters A-18 - A-25 shown in the following Table 6 (all of which esters were not
 commercially available but were prepared according to the third invention). The same evaluation as in
 Example 1 was made to obtain results as shown in the following Table 7.

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Table 6

Item Ester	Polyvalent alcohol	Monovalent fatty acid	Polybasic acid	Color (ASTM)	Dynamic viscosity at 40°C (cSt)
A-18	trimethylol ethane	2-ethylhexanoic acid (100)	—	L 0.5	17.9
A-19	trimethylol ethane	2-ethylhexanoic acid (95)	azelaic acid (5)	L 0.5	84.1
A-20	trimethylol ethane	2-ethylhexanoic acid (90)	sebacic acid (10)	L 0.5	105.4
A-21	trimethylol ethane	heptanoic acid (100)	—	L 0.5	15.1
A-22	trimethylol ethane	octanoic acid (50) isononanoic acid (50)	—	L 0.5	18.2
A-23	trimethylol ethane	nonanoic acid (70) isononanoic acid (30)	—	L 0.5	20.4
A-24	trimethylol propane	2-ethylhexanoic acid (100)	—	L 0.5	19.1
A-25	trimethylol propane	heptanoic acid (60) 2-ethylhexanoic acid (40)	—	L 0.5	15.4

Note) numerical value in parenthesis is mol% per total fatty acid

Table 7

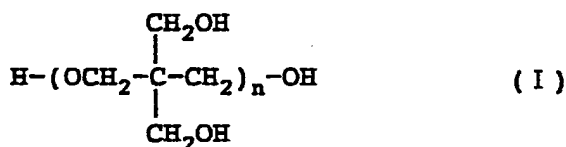
	Test lubricant	Dielectric constant at 80 °C (n° cm)	Two-phase separation temperature (° C)		Seizuring load (Kgfi)	Thermal stability				Hygroscopicity (water content, ppm)
			low temperature	high temperature		refrigerant R-12		refrigerant HFC-134a		
						color (ASTM)	sludge	color (ASTM)	sludge	
Acceptable Example	A-18	5.6 x 10 ¹²	≤-50	80≤	584	L 1.0	none	L 1.0	none	324
	A-19	1.9 x 10 ¹²	-30	80≤	612	L 1.0	none	L 1.0	none	368
	A-20	2.8 x 10 ¹²	-28	80≤	641	L 1.0	none	L 1.0	none	359
	A-21	7.6 x 10 ¹²	-41	80≤	541	L 1.0	none	L 1.0	none	317
	A-22	5.9 x 10 ¹²	≤-50	80≤	550	L 1.0	none	L 1.0	none	326
	A-23	3.1 x 10 ¹³	-38	80≤	581	L 1.0	none	L 1.0	none	333
	A-24	8.6 x 10 ¹²	≤-50	80≤	534	L 1.0	none	L 1.0	none	319
	A-25	4.3 x 10 ¹²	≤-50	80≤	519	L 1.0	none	L 1.0	none	321

As seen from Table 7, when the est rs according to the invention are compared with the conventional PGA (B-1 - B-3) shown in Tables 2 and 3, th electric insulating property represented by the dielectric constant is 100,000 times or mor and the two-phase separation at a high temperature is not caused. Furthermore, the seizing load is excellent and the hygroscopicity is low. The thermal stability is equal in case of the HFC-134a system, but is considerably excellent in case of the R-12 system.

Recently, HFC-134a causing substantially no breakage of ozone layer is closed up instead of R-12 widely used as a refrigerant in order to cope with the breakage of ozone layer through chlorofluorocarbon and hydrochlorofluorocarbon being a greatest problem in world-wide scale, but is poor in the compatibility with the conventional refrigeration lubricant, which is a bar for the development of replacement system. However, the refrigeration lubricants according to the invention have a sufficient compatibility with HFC-134a as a refrigerant and a high electric insulating property and also are excellent in the total performances, so that they have an effect that the conventional systems can be used as they are even when HFC-134a is used instead of the conventional R-12 and R-22 as a refrigerant.

Claims

1. A lubricant for hydrofluorocarbon refrigerant comprising as a main component an ester comprised of neopentyl glycol and at least one straight or branched-chain monovalent fatty acid having a carbon number of 3-18.
2. The lubricant according to claim 1, wherein at least one polybasic acid having a carbon number of 4-36 is further esterified in an amount of not more than 80 mol% per total fatty acid with said neopentyl glycol.
3. The lubricant according to claim 1, wherein said hydrofluorocarbon refrigerant is 1,1,1,2-tetrafluoroethane.
4. A lubricant for hydrofluorocarbon refrigerant comprising as a main component an ester comprised of at least one of pentaerythritol, dipentaerythritol and tripentaerythritol represented by the following general formula (I):



(in which n is 1, 2 or 3), and at least one straight or branched-chain monovalent fatty acid having a carbon number of 2-18.

5. The lubricant according to claim 4, wherein at least one polybasic acid having a carbon number of 4-36 is further esterified in an amount of not more than 80 mol% per total fatty acid.
6. The lubricant according to claim 4, wherein said hydrofluorocarbon refrigerant is 1,1,1,2-tetrafluoroethane.
7. A lubricant for hydrofluorocarbon refrigerant comprising as a main component an ester comprised of a polyvalent alcohol represented by the following general formula (II):



(in which R is an alkyl group having a carbon number of not more than 3), at least one straight or branched-chain monovalent fatty acid having a carbon number of 2-18, and not more than 25 mol% per total fatty acid of at least one polybasic acid having a carbon number of 4-36.

8. The lubricant according to claim 7, wherein said hydrofluorocarbon refrigerant is 1,1,1,2-tetrafluoroethane.



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EUROPEAN SEARCH REPORT

Application number

EP 89 11 9265

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl. 4)
X	US-A-3 878 112 (R.M. LUCK et al.) * Abstract; column 1, line 5 - column 4, line 3; claims 1,3 *	1,3,4	C 10 M 105/38 C 10 M 105/40 C 10 M 105/42 C 10 M 105/44// C 10 N 20:00 C 10 N 30:00 C 10 N 40:00
Y	--	2	
X	US-A-4 234 497 (M.L. HONIG) * Whole document *	1,4	
A	--	3	
X	INDUSTRIAL AND ENGINEERING CHEMISTRY, vol. 8, no. 1, March 1969, pages 70,71 H.F. LEDERLE: "Complex esters of 2,2-dimethylhydracrylic acid" * Whole article *	1	
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A	--	3	
X	US-A-4 113 642 (K.KOCH et al.) * Abstract; column 1, lines 6-24, 44 - column 4, line 12; examples 1-5,7; column 5, lines 14-20; claims 1-4,8 * -- ./.	5,7	
The present search report has been drawn up for all claims			
Place of search The Hague		Date of completion of the search 26-03-1990	Examiner FISCHER
CATEGORY OF CITED DOCUMENTS			
X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document		T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons A : member of the same patent family, corresponding document	



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CLAIMS INCURRING FEES

The present European patent application comprised at the time of filing more than ten claims.

- ☐ All claims fees have been paid within the prescribed time limit. The present European search report has been drawn up for all claims.
- ☐ Only part of the claims fees have been paid within the prescribed time limit. The present European search report has been drawn up for the first ten claims and for those claims for which claims fees have been paid.
- namely claims:
- ☐ No claims fees have been paid within the prescribed time limit. The present European search report has been drawn up for the first ten claims.

X LACK OF UNITY OF INVENTION

The Search Division considers that the present European patent application does not comply with the requirement of unity of invention and relates to several inventions or groups of inventions.

namely:

1. Claims 1-4
2. Claims 5,6
3. Claims 7,8

- ☒ All further search fees have been paid within the fixed time limit. The present European search report has been drawn up for all claims.
- ☐ Only part of the further search fees have been paid within the fixed time limit. The present European search report has been drawn up for those parts of the European patent application which relate to the inventions in respect of which search fees have been paid.
- namely claims:
- ☐ None of the further search fees has been paid within the fixed time limit. The present European search report has been drawn up for those parts of the European patent application which relate to the invention first mentioned in the claims.
- namely claims:



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EUROPEAN SEARCH REPORT

Application number

EP 89 11 9265

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl. 4)
Y	--	6, 8	
X	CHEMICAL ABSTRACTS, vol. 96, no. 10, March 1982, page 169, abstract 71653h, Columbus, Ohio, US; & JP-A-80 145 638 (NIPPON OILS AND FATS CO., LTD) 13-11-1980 * Whole abstract *	7	
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X	CHEMICAL ABSTRACTS, vol. 102, no. 2, January 1985, page 166, abstract 9492u, Columbus, Ohio, US; & JP-A- 59 164 393 (NIPPON OILS AND FATS CO., LTD) 17-09-1984 * Whole abstract *	7	TECHNICAL FIELDS SEARCHED (Int. Cl. 4)
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Y	--	6	
A	US-A-4 826 633 (D.D. CARR et al.) -----		
The present search report has been drawn up for all claims			
Place of search		Date of completion of the search	Examiner
CATEGORY OF CITED DOCUMENTS			
X : particularly relevant if taken alone		T : theory or principle underlying the invention	
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P : intermediate document		& : member of the same patent family, corresponding document	